How to select the right deck using load and diaphragm tables

Roof Decks - Types B, BI, BV, BIV

ASD

Selecting the appropriate deck for your building project is not a standard decision. Looking at load and diaphragm tables to select the right deck for your application can significantly reduce costs.

| | | PROPE | RTIES | | | SECTION P | ROPERTIES | | | DESIGN | STRENGTHS | | Rbi/Ω | | | |
|------|-------------------------|-------------------|--------------------|-----------------|---|---|---|---|-----------------------|-----------------------|-------------------|--------------------|--------------------|--|--|--|
| Gage | F _y (ksi) | Coverage (in.) | Thickness (in.) | Weight (psf) | I _p (in. ⁴ /ft.) | I _n (in. ⁴ /ft.) | S _p (in. ³ /ft.) | S _n (in. ³ /ft.) | Mn,p/Ω (inlb./ft.) | Mn,n/Ω (inlb./ft.) | Vn/Ω (lb./ft.) | Rbe/Ω (lb./ft.) | Rbi/Ω (lb./ft.) | | | |
| 22 | 33 | 36 | 0.0295 | 1.63 | 0.162 | 0.175 | 0.183 | 0.189 | 3626 | 3734 | 1738 | 539 | 974 | | | |
| 20 | 33 | 36 | 0.0358 | 1.98 | 0.205 | 0.213 | 0.227 | 0.238 | 4484 | 4712 | 2100 | 769 | 1399 | | | |
| 18 | 33 | 36 | 0.0474 | 2.62 | 0.281 | 0.281 | 0.307 | 0.315 | 6073 | 6233 | 2761 | 1285 | 2358 | | | |
| 16 | 33 | 36 | 0.0598 | 3.30 | 0.355 | 0.355 | 0.393 | 0.395 | 7757 | 7800 | 3456 | 1964 | 3627 | | | |

Section properties are calculated in accordance with the AISI Cold-Formed Steel Design Specifications, 2007 Edition.
 Rbe/Q and Rbi/Q values are based on minimum bearing lengths of 1.5" for end bearing and 3" for interior bearing.

| Span Condition | Gage | | | | | Max. | | | | | | |
|-------------------|------|-----------|-----------|-----------|-----------|--------------------------------|---------|---------|---------|---------|-------------|---------------|
| | | | | | | Center to Center Span (ft in.) | | | | | Constr. Spa | |
| | | 4 - 0 | 5 - 0 | 6 - 0 | 7 - 0 | 8 - 0 | 9 - 0 | 10 - 0 | 11 - 0 | 12 - 0 | 13 - 0 | (Ctr. to Ctr. |
| | 22 | 151 / 165 | 97 / 85 | 67 / 49 | 49 / 31 | - | - | 1-1 | - | 120 | - | 6' - 0" |
| Single | 20 | 187 / 210 | 120 / 108 | 83 / 62 | 61 / 39 | 47 / 26 | - | (5) | - | - | | 7' - 5" |
| Single | 18 | 253 / 288 | 162 / 147 | 112 / 85 | 83 / 54 | 63 / 36 | 50 / 25 | 40 / 18 | 33 / 14 | - | - | 10' - 1" |
| | 16 | 323 / 363 | 207 / 186 | 144 / 108 | 106 / 68 | 81 / 45 | 64 / 32 | 52 / 23 | 43 / 17 | 36 / 13 | 31 / 11 | 12' - 11" |
| | 22 | 152 / 416 | 98 / 213 | 68 / 123 | 50 / 78 | 39 / 52 | | - | | * 1 | 18 | 7' - 3" |
| Double | 20 | 191 / 516 | 124 / 264 | 86 / 153 | 64 / 96 | 49 / 65 | 39 / 45 | 31 / 33 | - | 120 | - | 9' - 0" |
| Double | 18 | 253 / 695 | 163 / 356 | 114 / 206 | 84 / 130 | 65 / 87 | 51 / 61 | 41 / 44 | 34 / 33 | 29 / 26 | 25 / 20 | 12' - 2" |
| | 16 | 317 / 876 | 205 / 448 | 143 / 260 | 105 / 163 | 81 / 109 | 64 / 77 | 52 / 56 | 43 / 42 | 36 / 32 | 31 / 26 | 15' - 6" |
| | 22 | 188 / 325 | 122 / 167 | 85 / 96 | 63 / 61 | 48 / 41 | | 150 | | 157 | (IE) | 7' - 4" |
| Triple | 20 | 236 / 404 | 153 / 207 | 107 / 120 | 79 / 75 | 61 / 50 | 48 / 35 | 39 / 26 | - | - | 12 | 9' - 1" |
| riple | 18 | 312 / 544 | 203 / 278 | 142 / 161 | 105 / 101 | 80 / 68 | 64 / 48 | 52 / 35 | 43 / 26 | 36 / 20 | 31 / 16 | 12' - 4" |
| | 16 | 391 / 685 | 254 / 351 | 177 / 203 | 131 / 128 | 101 / 86 | 80 / 60 | 65 / 44 | 53 / 33 | 45 / 25 | 38 / 20 | 15' - 9" |

This table shows standard allowable uniform load time and maximum construction span. Both of which are dependent on deck type and span condition. Construction spans and uniform loads are based on ANSI/SDI RD-2010 Standard for steel roof deck.

When selecting deck for particular projects there are many variables to consider such as, depth, costs, and attachment, among others. It is always beneficial to select the most economical deck type and gauge, whether it is roof or floor deck. To guide this decision, the Steel Deck Institute standardizes the gauge and yield stress of the material so that the most economical would mean the thinnest gauge and lowest yield strength for the design of the specific project. To help you make sense of the tables, New Millennium has developed a steel deck design tool to further guide you.

To get started, use the following questions as a guide to find the deck that meets your project needs:

- Is the project load and resistance factor design (LRFD) or allowable strength design (ASD)?
- What is the maximum loading for the deck area?
- What is the maximum span for this area? (You can use a smaller gauge for triple span conditions.)
- If this is floor deck, what is the construction loading?
 (LW or NW concrete, slab depth, method of placement, and finishing, etc.)
- What are the required deflection limits?
- What is the required diaphragm capacity?

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DID YOU KNOW? (continued)

After answering the questions on the preceding page, review the deck load tables and locate the appropriate span and condition. If the desired gauge is not adequate for the uniform total load or the required deflection, an increase in gauge thickness may be required. Note that the deflection requirements can still be checked on the load tables by multiplying the load for the deflection listed by the appropriate factor. The allowable loading will increase with the rising gauge thickness. Additionally, the maximum construction span must be greater than the maximum spacing in the area to avoid shoring. If the required load is greater than the largest allowable load on the table, then a deeper deck profile and/or thicker slab for floors may be needed.

which include shear strengths. Note that the capacities given in diaphragm tables are nominal strengths. These strengths must be multiplied by the appropriate resistance factor or divided by the appropriate safety factor listed in the upper right corner or in the table. These tables can be used once the deck type and gauge have been selected to design the attachment for the required diaphragm. Minimum bearing lengths, published in the table notes, should be verified to meet project conditions. If the minimum bearing lengths are not met, it will require another check for web crippling. Web crippling is the check for local buckling due to the shear force in the deck.

Selecting diaphragm

Diaphragm capacities can be approached in the same manner of using tables. If additional strength is needed for floor decks, refer to New Millennium's diaphragm tables,

Learn more about the steel deck design tool and download the tables: www.newmill.com/bim-design-tools/tools/steel-decking-tools.html.

| Support Fa | , Design Thick steners: 5/8" p asteners: #10 | puddle welds | _ | | | | | | | | | | Φ (WINE Φ (Other Φ (Buckling | r): 0.60 | Ω | (WIND): 2.35 (Other): 2.65 ickling): 2.00 | |
|---------------------|--|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------------------------------------|----------------|-------|---|---|
| Support Fastener | Side Lap Conn. | | | | | | Ce | in.) | | | | | | K ₁ | | | |
| Pattern | per Span | 4 - 0 | 4 - 6 | 5 - 0 | 5 - 6 | 5 - 9 | 6 - 0 | 6 - 3 | 6 - 6 | 6 - 9 | 7 - 0 | 7 - 6 | 8 - 0 | 8 - 6 | 9 - 0 | (ft. ⁻¹) | 1 |
| | 0 | 1671 | 1493 | 1334 | 1205 | 1149 | 1097 | 1050 | 1006 | 966 | 928 | 860 | 801 | 749 | 702 | 0.357 | 1 |
| | 1 | 1827 | 1649 | 1488 | 1345 | 1283 | 1225 | - | - | - | - | - | - | - | - | 0.299 | Typical noi |
| 36/9 Dn = 68 | 2 | 1977 | 1789 | 1631 | 1485 | 1416 | 1354 | 1296 | 1243 | 1193 | 1148 | 1065 | 993 | 929 | 873 | 0.258 | |
| | 3 | 2121 | 1924 | 1757 | 1616 | 1550 | 1482 | 1419 | 1361 | 1307 | 1257 | 1168 | 1089 | 1020 | 958 | 0.226 | |
| | 4 | 2258 | 2054 | 1880 | 1732 | 1665 | 1604 | 1542 | 1479 | 1421 | 1367 | 1270 | 1185 | 1110 | 1044 | 0.202 | |
| | 5 | 2388 | 2178 | 1999 | 1844 | 1775 | 1710 | 1650 | 1593 | 1535 | 1477 | 1373 | 1281 | 1201 | 1129* | 0.182 | |
| | 6 | 2512 | 2298 | 2113 | 1953 | 1881 | 1814 | 1751 | 1692 | 1636 | 1584 | 1475 | 1377* | 1291* | 1214* | 0.166 | |
| | 7 | 2630 | 2413 | 2224 | 2059 | 1985 | 1915 | 1850 | 1788 | 1731 | 1676 | 1577* | 1473* | 1382* | 1300* | 0.152 | |
| | 8 | 2741 | 2522 | 2330 | 2161 | 2085 | 2013 | 1946 | 1882 | 1822 | 1766 | 1662* | 1569* | 1472* | 1385* | 0.141 | |
| | 9 | 2847 | 2627 | 2432 | 2260 | 2182 | 2109 | 2039 | 1974 | 1912 | 1854* | 1747* | 1650* | 1562* | 1471* | 0.131 | |
| | 10 | 2947 | 2726 | 2530 | 2356 | 2276 | 2201 | 2130 | 2063 | 2000* | 1940* | 1829* | 1730* | 1640* | 1556* | 0.122 | |
| | 0 | 1038 | 918 | 822 | 743 | 709 | 678 | 649 | 622 | 597 | 574 | 533 | 497 | 465 | 437 | 0.535 | is depende and attach diaphragn the table n appropria |
| | 1 | 1219 | 1089 | 976 | 883 | 843 | 806 | - | 2 | - | 12 | 121 | 2 | | 10 | 0.415 | |
| | 2 | 1384 | 1245 | 1129 | 1023 | 976 | 934 | 895 | 859 | 825 | 794 | 738 | 689 | 646 | 608 | 0.340 | |
| | 3 | 1542 | 1391 | 1265 | 1159 | 1110 | 1062 | 1018 | 977 | 939 | 904 | 841 | 785 | 737 | 693 | 0.287 | |
| 36/7 | 4 | 1693 | 1531 | 1396 | 1282 | 1231 | 1184 | 1140 | 1095 | 1053 | 1014 | 943 | 881 | 827 | 779 | 0.249 | |
| | 5 | 1836 | 1666 | 1522 | 1400 | 1346 | 1295 | 1248 | 1204 | 1163 | 1123 | 1046 | 977 | 917 | 864 | 0.219 | the appro |
| Dn = 68 | 6 | 1971 | 1795 | 1644 | 1515 | 1458 | 1404 | 1354 | 1307 | 1263 | 1222 | 1147 | 1074 | 1008 | 949 | 0.196 | me uppn |

Typical nominal diaphragm shear strength table. Diaphragm s dependent on the deck type and attachment pattern. All diaphragm capacitates from the table must be divided by the appropriate Ω or multiplied by the appropriate Ω or multiplied by the appropriate Ω or multiplied.



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